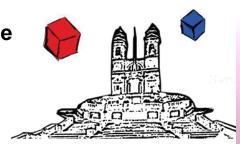




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# Flight Experimentation with Magnetic Attitude Control System of SiriusSat-1&2 Nanosatellites

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#### Content

- SiriusSat-1&2 details
- On-flight sensors calibration
- Attitude and magnetometer bias estimation
- Algorithms testing results
- Conclusions



#### Nanosatellites SiriusSat-1&2

#### SiriusSat-1&2

- assembled by school students in a collaboration with SPUTNIX specialists
- educational and space weather monitoring 1U CubeSats

#### **Attitude control system:**

active magnetic: air core magnetorquers inbuilt in solar panels

#### **Attitude sensors:**

- magnetometer
- angular velocity sensor

#### **Inertia tensor and mass:**

$$J = \begin{bmatrix} 6.9 & 0.3 & 0 \\ 0.3 & 6.9 & 0 \\ 0 & 0 & 2.9 \end{bmatrix}$$

$$J = \begin{bmatrix} 6.9 & 0.3 & 0 \\ 0.3 & 6.9 & 0 \\ 0 & 0 & 2.9 \end{bmatrix} \cdot 10^{-3} \text{kg} \cdot \text{m}^2; \quad m = 1.45 \text{ kg}$$
Magnetic Attitude Control System of SiriusSat-1



Photo of the SiriusSat-1&2



#### **ADCS** parameters

- The SiriusSats satellites consist of:
  - main stack of electronic devices
  - an assembly frame
  - solar panels
- The on-board computer module SXC-MB-04 contains the following set of devices:
  - slot for the Raspberry-Pi CM3 processor
  - power supply system
  - angular velocity sensor and magnetometer
  - control unit for magnetorquers



Solar panels and inbuilt air core magnetic coils

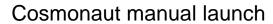


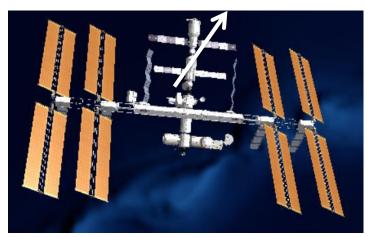
On-board computer SXC-MB-04

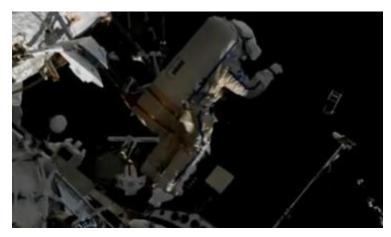


## Launch on August 15, 2018

The direction of the SiruisSat-1&2 launch from ISS











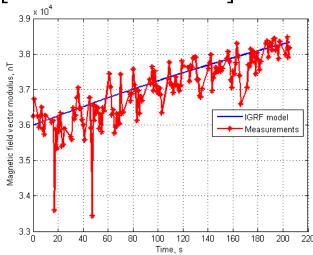
### Magnetometer calibration

Magnetometer measurement model:

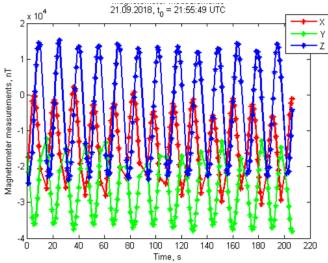
$$\mathbf{B}_{meas} = \mathbf{A}\mathbf{B}_{orb} + \Delta\mathbf{B} + \delta\mathbf{B}$$

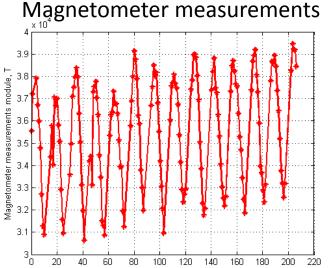
 Comparing the magnitude with IGRF geomagnetic field model value the magnetometer bias obtained

$$\Delta \mathbf{B} = \begin{bmatrix} 4.98 & -0.56 & -4.71 \end{bmatrix} \cdot 10^3 \,\mathrm{nT}$$



Geomagnetic field calculated using IGRF and magnetometer measurements without bias





Magnetometer measurements value



## Attitude motion reconstruction technique

Motion equations

$$\mathbf{J}\dot{\mathbf{\Omega}} + \mathbf{\Omega} \times \mathbf{J}\mathbf{\Omega} = \mathbf{M}_{mag} + \mathbf{M}_{grav}$$

$$\mathbf{B}_{meas} = \mathbf{A}\mathbf{B}_o + \mathbf{B}_{bias}$$

$$\dot{\Lambda} = \frac{1}{2} \mathbf{C} \Lambda \qquad \Lambda = (\mathbf{q}, q_0)$$

Initial conditions vector

$$\boldsymbol{\xi} = \left[ q_1(t=0), q_2(t=0), q_{3,}(t=0), \omega_1(t=0), \omega_2(t=0), \omega_3(t=0) \right]^T$$

The problem of the vector of initial conditions determination reduces to the problem of the following function minimization

$$\Phi(\boldsymbol{\xi}) = \sum_{k=1}^{N} \left( \left| \tilde{\mathbf{b}}_{\text{model}}^{k} - \mathbf{b}_{meas}^{k} \right| \right)^{2}$$

 $\mathbf{b}_{meas}^{i}$  is the unit vector along the geomagnetic field calculated using measurements after excluding the constant bias

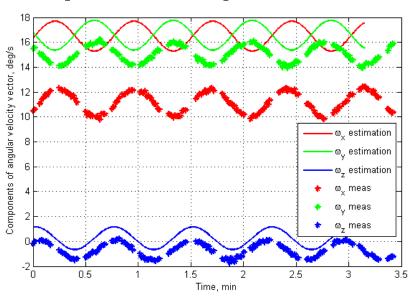
 $\tilde{\mathbf{b}}_{\text{mod }el}^{i}$  is the unit vector along the geomagnetic field calculated IGRF model



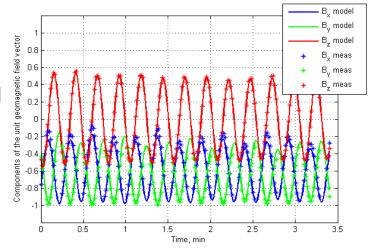
## Measurements processing results

- Using magnetometer measurements the attitude motion is reconstructed
- Angular velocity sensor measurements are shifted relative to the estimated angular velocity
- The sensor bias is

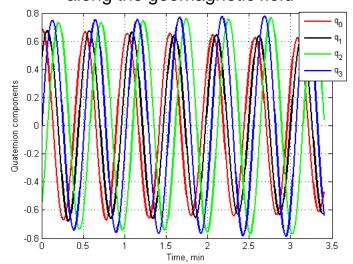
$$\Delta \mathbf{\omega} = \begin{bmatrix} 5.94 & 1.72 & 1.28 \end{bmatrix}^T \text{ deg/s}$$



Angular velocity vector and angular velocity sensor measurements



Measured and predicted unit vector along the geomagnetic field





### Magnetic control algorithms

Magnetic three-axis attitude control to be tested

$$\mathbf{m} = -k_{\omega}\mathbf{B} \times \mathbf{\Omega} - k_{a}\mathbf{B} \times \mathbf{S}$$

- Real-time attitude determination is necessary
- Magnetometer bias as well as angular velocity sensor bias are changing due to the onboard magnetic sources
- Extended Kalman filter using the magnetometer measurements is applied to the problem
- Magnetometer bias is included in the state vector

State vector of the system

$$\mathbf{x} = [\mathbf{q}, \, \mathbf{\Omega}, \, \Delta \mathbf{B}]^T$$

Linearized motion equations

$$\delta \dot{\mathbf{x}}(t) = \mathbf{F}(t) \delta \mathbf{x}(t)$$

Dynamics matrix

$$\mathbf{F} = \begin{pmatrix} -\mathbf{W}_{\Omega} & \frac{1}{2}\mathbf{E} & \mathbf{0}_{3x3} \\ \mathbf{J}^{-1}\mathbf{F}_{qw} & \mathbf{J}^{-1}(\mathbf{F}_{gir}^{\Omega} - \mathbf{W}_{\mathbf{A}\mathbf{\omega}_{orb}}\mathbf{J}) & \mathbf{0}_{3x3} \\ \mathbf{0}_{3x3} & \mathbf{0}_{3x3} & \mathbf{0}_{3x3} \end{pmatrix}$$

Measurement model

$$\mathbf{z} = \mathbf{A}\mathbf{B}_{orb} + \Delta\mathbf{B} + \mathbf{\eta}_{V},$$

Linearized measurement model

$$\delta \mathbf{z} = -2\mathbf{W}_{\delta \mathbf{q}} \hat{\mathbf{B}} = -2\mathbf{W}_{\hat{\mathbf{B}}} \delta \mathbf{q}$$

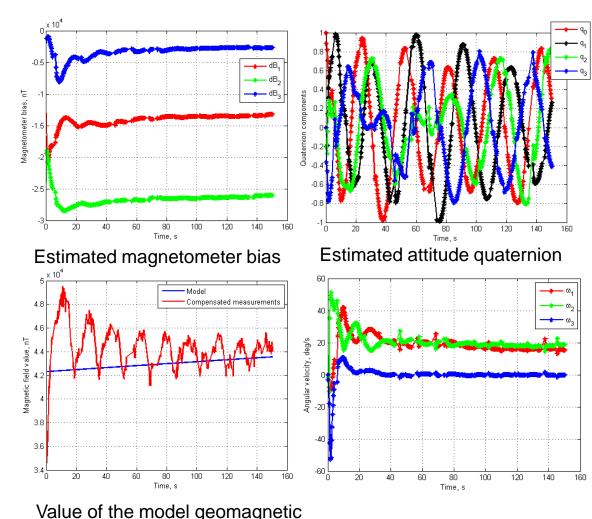
Measurement matrix

$$\mathbf{H} = \begin{bmatrix} -2\mathbf{W}_{\hat{\mathbf{B}}} & \mathbf{0}_{3x3} & \mathbf{E}_{3x3} \end{bmatrix}$$



## **EKF Testing Using Engineering Model**

- Implemented EKF using the magnetometer measurements obtained on August 06, 2019
- State vector estimations converged close to real values
- Magnetometer bias is estimated with 1000 nT accuracy
- The attitude motion estimation accuracy is about 3 deg
- This accuracy is enough for coarse three-axis attitude control



Estimated angular velocity

field vector



#### Conclusions

- Results of the angular motion analysis using the telemetry data are discussed
- The algorithm is proposed for the attitude motion and magnetometer bias estimation in real time
- The algorithm is tested using the hardware-in-the-loop technique
- Real flight data was successfully processed by the onboard computer identical to the one installed on SiriusSat satellites
- The relevant software is currently uploaded via the UHF antenna

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## Thank you for attention!

Our web-site: http://keldysh.ru/microsatellites/eng/



